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CETA 82-4

Hand-Held Calculator Algorithms for Coastal Engineering (Second Series)

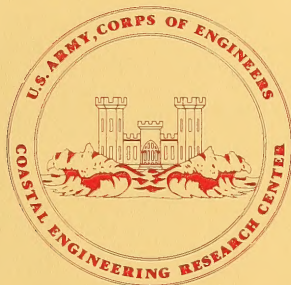
by

Todd L. Walton, Jr.

WHOI
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COLLECTION

COASTAL ENGINEERING TECHNICAL AID NO. 82-4

NOVEMBER 1982



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U.S. ARMY, CORPS OF ENGINEERS
COASTAL ENGINEERING
RESEARCH CENTER

Kingman Building
Fort Belvoir, Va. 22060

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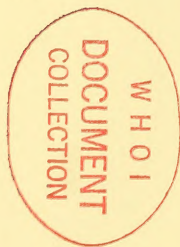
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| REPORT DOCUMENTATION PAGE | | READ INSTRUCTIONS BEFORE COMPLETING FORM | | | | |
|---|-----------------------|--|-----------------------|-----------------|---------------------|----------------------|
| 1. REPORT NUMBER CETA 82-4 | 2. GOVT ACCESSION NO. | 3. RECIPIENT'S CATALOG NUMBER | | | | |
| 4. TITLE (and Subtitle) HAND-HELD CALCULATOR ALGORITHMS FOR COASTAL ENGINEERING (Second Series) | | 5. TYPE OF REPORT & PERIOD COVERED Coastal Engineering Technical Aid | | | | |
| | | 6. PERFORMING ORG. REPORT NUMBER | | | | |
| 7. AUTHOR(s) Todd L. Walton, Jr. | | 8. CONTRACT OR GRANT NUMBER(s) | | | | |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS Department of the Army Coastal Engineering Research Center (CEREN-EV) Kingman Building, Fort Belvoir, Virginia 22060 | | 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS C31181 | | | | |
| 11. CONTROLLING OFFICE NAME AND ADDRESS Department of the Army Coastal Engineering Research Center Kingman Building, Fort Belvoir, Virginia 22060 | | 12. REPORT DATE November 1982 | | | | |
| 14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) | | 13. NUMBER OF PAGES 41 | | | | |
| | | 15. SECURITY CLASS. (of this report) UNCLASSIFIED | | | | |
| | | 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE | | | | |
| 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. | | | | | | |
| 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) | | | | | | |
| 18. SUPPLEMENTARY NOTES | | | | | | |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) | | | | | | |
| <table border="0"> <tr> <td>Calculator algorithms</td> <td>Wave generation</td> </tr> <tr> <td>Coastal engineering</td> <td>Wave transformations</td> </tr> </table> | | | Calculator algorithms | Wave generation | Coastal engineering | Wave transformations |
| Calculator algorithms | Wave generation | | | | | |
| Coastal engineering | Wave transformations | | | | | |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) | | | | | | |
| <p>This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation. Six programs are included for use with HP41CV hand-held calculators which employ the Reverse Polish Notation (RPN). These programs can be used to compute linear wave parameters, orbital velocities, breaking wave height and direction, shallow-water wave forecasts, depth-limited breaking wave height, and wave transmission past a vertical barrier.</p> | | | | | | |

PREFACE

This report provides coastal engineers a second series of algorithms for a number of hand-held calculator programs for coastal engineering, primarily in the area of wave transformations and wave generation. These algorithms were developed under the U.S. Army Coastal Engineering Research Center's (CERC) Littoral Data Collection Methods and Their Engineering Application work unit, Shore Protection and Restoration Program, Coastal Engineering Area of Civil Works Research and Development.

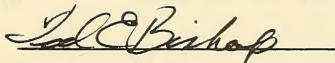
The report was prepared by Dr. Todd L. Walton, Jr., Hydraulic Engineer, under the general supervision of Dr. J.R. Weggel, Chief, Evaluation Branch, and Mr. N. Parker, Chief, Engineering Development Division.

The author acknowledges the assistance of J. Dean in preparing the manuscript. The review by Dr. J.R. Weggel is appreciated.

Technical Director of CERC was Dr. Robert W. Whalin, P.E., upon publication of this report.

Comments on this publication are invited.

Approved for publication in accordance with Public Law 166, 79th Congress, approved 31 July 1945, as supplemented by Public Law 172, 88th Congress, approved 7 November 1963.



TED E. BISHOP
Colonel, Corps of Engineers
Commander and Director

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CONVERSION FACTORS, U.S. CUSTOMARY TO METRIC (SI) UNITS OF MEASUREMENT

U.S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

| Multiply | by | To obtain |
|--------------------|-------------------------|---|
| inches | 25.4 | millimeters |
| | 2.54 | centimeters |
| square inches | 6.452 | square centimeters |
| cubic inches | 16.39 | cubic centimeters |
| feet | 30.48 | centimeters |
| | 0.3048 | meters |
| square feet | 0.0929 | square meters |
| cubic feet | 0.0283 | cubic meters |
| yards | 0.9144 | meters |
| square yards | 0.836 | square meters |
| cubic yards | 0.7646 | cubic meters |
| miles | 1.6093 | kilometers |
| square miles | 259.0 | hectares |
| knots | 1.852 | kilometers per hour |
| acres | 0.4047 | hectares |
| foot-pounds | 1.3558 | newton meters |
| millibars | 1.0197×10^{-3} | kilograms per square centimeter |
| ounces | 28.35 | grams |
| pounds | 453.6 | grams |
| | 0.4536 | kilograms |
| ton, long | 1.0160 | metric tons |
| ton, short | 0.9072 | metric tons |
| degrees (angle) | 0.01745 | radians |
| Fahrenheit degrees | 5/9 | Celsius degrees or Kelvins ¹ |

¹To obtain Celsius (C) temperature readings from Fahrenheit (F) readings, use formula: $C = (5/9) (F - 32)$.

To obtain Kelvin (K) readings, use formula: $K = (5/9) (F - 32) + 273.15$.

HAND-HELD CALCULATOR ALGORITHMS FOR COASTAL ENGINEERING (Second Series)

by
Todd L. Walton, Jr.

I. INTRODUCTION

The advent of the hand-held programable calculator has led to the development of numerous programs in various fields of engineering and science. Coastal engineering is no exception. This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation.

There are basically two types of hand-held programable calculators: those that use algebraic logic, such as Texas Instruments, Algebraic Operating System (AOS) notation, and those that use Reverse Polish Notation (RPN), such as Hewlett-Packard. The six programs presented herein are versions of RPN logic suitable for use on HP41CV programable calculators with or without accessory printer. Each program is documented, the assumptions are briefly described, and references to more detailed presentations of the theory are given. This same set of algorithms was programmed for the TI-59 (AOS logic) and HP67 (RPN logic) calculators in an earlier report with the same title (Walton, Birkemeier, and Weggel, 1982)¹.

Each of the RPN programs incorporates HP41 compatible print routines which print and label all input and output parameters. The user only has to enter the input parameters and the results are automatically computed and printed. Since the printing routines increase program length by as much as 25 percent, use of a magnetic card for permanent program storage is recommended. All print steps are marked with asterisks and need not be entered if printing is not desired.

II. PROGRAMS

Six programs (100, 101, 102, 103, 104, and 105) are presented in this report. Program 100, a simple program that computes linear wave theory wavelength for a given depth, is designed to be used as the basis for any program that requires wavelength; in fact, it has been incorporated into programs 101, 102, and 105.

Program 101 is another basic program which computes not only wavelength but also a number of other linear wave theory parameters. This program forms the basis for program 102 and can be adapted to other programs as well.

¹WALTON, T.L., BIRKEMEIER, W.A., and WEGGEL, J.R., "Hand-Held Calculator Algorithms for Coastal Engineering," CETA 82-1, U.S. Army, Corps of Engineers, Coastal Engineering Research Center, Fort Belvoir, Va., Jan. 1982.

Program 102 computes linear wave parameters and breaking wave height and direction based on nearshore or deepwater wave information. Program 103 can be used to forecast wave height and period in shallow water. Program 104 and 105 address wave conditions at structures--program 104 predicts the depth-limited design breaking wave height at a structure; 105 uses Fuchs' equation to predict wave transmission over a thin barrier.

Each program allows either English or metric input and output. Program listings are annotated, making it possible to follow the logic of the algorithm and to make modifications if desired.

There are undoubtedly many calculator programs not included here that have been developed on coastal engineering subjects. Practicing engineers who would like to disseminate such programs (in either AOS or RPN) to other users are encouraged to submit them to the Coastal Engineering Research Center (CERC). If the response is great enough, additional reports presenting the programs will be prepared. Comments, programs, or suggestions for programs should be sent to:

Commander and Director
US Army Coastal Engineering Research Center
ATTN: Evaluation Branch
Kingman Building
Fort Belvoir, VA 22060

These programs and future programs will generally correspond to the following numbering scheme:

| | |
|--------------------|----------|
| Miscellaneous | 0-99 |
| Waves and currents | 100-299 |
| Inlets | 300-499 |
| Beaches | 500-699 |
| Geology | 700-899 |
| Structures | 900-1099 |

In general, the documentation of programs submitted should be in a format paralleling that of the programs presented in this report. A blank set of forms which can be reproduced is included in the Appendix.

Program Description

| | | | |
|----------------------|---|-----------------|----------|
| Program Title | 100R-41CV Linear Wave Theory Wavelength (RPN Logic) | | |
| Name | T.L. Walton, Jr. | Date | 1/82 |
| Address | Coastal Engineering Research Center | | |
| City | Kingman Building | State | Virginia |
| | Fort Belvoir, | Zip Code | 22060 |

Program Description, Equations, Variables, etc.

This algorithm takes deepwater wavelength as input and using the depth at a given site iterates to obtain wavelength by linear wave theory. Algorithm uses English or metric system of units.

REFERENCE

U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER,
Shore Protection Manual, 3d ed., Vol. I, Eq. (2-4), Stock No. 008-
022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977.

Operating Limits and Warnings

100R-41CV-1

User Instructions

100R-41CV LINEAR THEORY WAVELENGTH (RPN LOGIC)

SIZE: 011

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|------|------------------------------|-----------|---------------|-----------|
| 1 | LOAD PROGRAM (WAVEL) | | [XEQ] "WAVEL" | E OR M? |
| | | | | |
| | TO CALCULATE L IN ENGLISH | UNITS: | | |
| 2 | PRESS GTO "E" | | GTO "E" | |
| 3 | PRESS R/S | | [R/S] | PERIOD? |
| 4 | ENTER PERIOD T, PRESS R/S | T(sec) | [R/S] | DEPTH? |
| 5 | ENTER DEPTH D, PRESS R/S | d (ft) | [R/S] | L (ft) |
| | | | | |
| | TO CALCULATE L IN METRIC | UNITS: | | |
| 2a | PRESS GTO "M" | | GTO "M" | |
| 3a | PRESS R/S | | [R/S] | PERIOD? |
| 4a | ENTER PERIOD T, PRESS R/S | T(sec) | [R/S] | DEPTH? |
| 5a | ENTER DEPTH D, PRESS R/S | d(meters) | [R/S] | L(meters) |
| | | | | |
| | | | | |
| | Example 1 and 1a | | | |
| | T = 10sec , d = 10ft (3.05m) | | | |
| | ENGLISH AND METRIC PRINTOUTS | | | |
| | ENGLISH | | | |
| | PERIOD= | | | |
| | 10.0000 *** | | | |
| | DEPTH= | | | |
| | 10.0000 *** | | | |
| | LENGTH= | | | |
| | 175.7738 *** | | | |
| | | | | |
| | | | | |
| | METRIC | | | |
| | PERIOD= | | | |
| | 10.0000 *** | | | |
| | DEPTH= | | | |
| | 3.0500 *** | | | |
| | LENGTH= | | | |
| | 53.6063 *** | | | |
| | note: " = [ALPHA] | | | |

100R-41CV-2

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|--------------|----------|---------------------------------|------|--------------|----------|---|
| 01 | LBL "WAVE" | | | 57 | E+X | | |
| 02 | "E OR M ?" | | | 58 | + | | |
| 03 | PROMPT | | | 59 | / | | $\tanh \frac{2nd}{L_{old}}$ |
| 04 | LBL E | | | 60 | RCL 01 | | |
| 05 | 32.2 | | | 61 | * | | $L' = L_0 \tanh \left(\frac{2nd}{L_{old}} \right)$ |
| 06 | STO 06 | | $g(English) \rightarrow R_{06}$ | 62 | RCL 03 | | |
| 07 | "ENGLISH" | | | 63 | + | | |
| 08 | PRA | | | 64 | 2 | | |
| 09 | GTO 01 | | | 65 | / | | |
| 10 | LBL "M" | | | 66 | STO 02 | | $\frac{L' + L_{old}}{2} \rightarrow R_2$ |
| 11 | "METRIC" | | | 67 | RCL 03 | | |
| 12 | PRA | | | 68 | - | | |
| 13 | 9.81 | | | 69 | ABS | | ϵ (error tolerance) 1 ft or 1 meter |
| 14 | STO 06 | | $g(metric) \rightarrow R_{06}$ | 70 | 1 | | |
| 15 | LBL 01 | | | 71 | X/Y? | | |
| 16 | "PERIOD=" | | | 72 | GTO 05 | | |
| 17 | PRA | | | 73 | RCL 02 | | |
| 18 | "PERIOD?" | | | 74 | GTO "ITERAT" | | |
| 19 | PROMPT | | | 75 | LBL 05 | | |
| 20 | PRX | | | 76 | RCL 02 | | L in display |
| 21 | STO 07 | | $T \rightarrow R_{07}$ | 77 | "LENGTH=" | | |
| 22 | X+2 | | | 78 | PRA | | |
| 23 | RCL 06 | | | 79 | PRX | | |
| 24 | * | | | 80 | STOP | | |
| 25 | 2 | | | 81 | END | | |
| 26 | / | | | | | | |
| 27 | PI | | | | | | |
| 28 | / | | | | | | |
| 29 | STO 01 | | $L_0 \rightarrow R_{01}$ | | | | |
| 30 | "DEPTH=" | | | | | | |
| 31 | PRA | | | | | | |
| 32 | "DEPTH?" | | | | | | |
| 33 | PROMPT | | | | | | |
| 34 | PRX | | | | | | |
| 35 | ENTER+ | | | | | | |
| 36 | 2 | | | | | | |
| 37 | * | | | | | | |
| 38 | PI | | | | | | |
| 39 | * | | | | | | |
| 40 | STO 05 | | $2nd \rightarrow R_{05}$ | | | | |
| 41 | RCL 01 | | | | | | |
| 42 | LBL "ITERAT" | | | | | | |
| 43 | STO 03 | | $L_{old} \rightarrow R_{03}$ | | | | |
| 44 | 1/X | | | | | | |
| 45 | RCL 05 | | | | | | |
| 46 | * | | | | | | |
| 47 | STO 04 | | | | | | |
| 48 | E+X | | | | | | |
| 49 | RCL 04 | | | | | | |
| 50 | CHS | | | | | | |
| 51 | E+X | | | | | | |
| 52 | - | | | | | | |
| 53 | RCL 04 | | | | | | |
| 54 | E+X | | | | | | |
| 55 | RCL 04 | | | | | | |
| 56 | CHS | | | | | | |

100R-41CV-3

* THESE STEPS MUST BE DELETED IF NO PRINTER IS AVAILABLE

Program Description

| | | | |
|---------------|---|----------|----------|
| Program Title | 101R-41CV Calculation of Wave Parameters from Linear Theory (RPN Logic) | | |
| Name | T.L. Walton, Jr. | | 1/82 |
| Address | Coastal Engineering Research Center | | |
| City | Kingman Building | State | Virginia |
| | Fort Belvoir, | Zip Code | 22060 |

Program Description, Equations, Variables, etc.

This program calculates the product of the wave number and depth, kd , the ratio of group wave speed to wave celerity, $n = 0.5 (1+2kd/\sinh 2kd)$, the group wave speed, C_g , the shoaling coefficient, K_s , the refraction coefficient, K_r , horizontal orbital velocity, u , and vertical orbital velocity, w .

Program input includes wave period, T , deepwater wave angle, α_0 , deepwater wave height, H_0 , wave phase angle, θ , depth of water, d , at which results are desired, and depth from surface, z , at which velocities are calculated. This program assumes straight and parallel offshore bottom contours for assumption of Snell's law of refraction. Algorithm uses English or metric system of units.

REFERENCE

U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, *Shore Protection Manual*, 3d ed., Vol. I, Ch. 2, Stock No. 008-022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977.

Operating Limits and Warnings

If printer is not used, R/S must be inserted where output values are desired (i.e., where printer output steps are deleted).

101R-41CV-1

User Instructions

101R-41CV CALCULATION OF WAVE PARAMETERS FROM LINEAR THEORY (RPN LOGIC) SIZE: 021

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|------|---|------------------|----------------|----------------|
| 1 | LOAD PROGRAM (LINEAR) | | [XEQ] "LINEAR" | E OR M? |
| | | | | |
| | TO COMPUTE IN ENGLISH UNITS: | | | |
| 2 | PRESS GTO "E" | | GTO "E" | |
| 3 | PRESS R/S | | [R/S] | PERIOD? |
| 4 | ENTER PERIOD T, PRESS R/S | T(sec) | [R/S] | DEPTH? |
| 5 | ENTER DEPTH D, PRESS R/S | d (ft.) | [R/S] | AO? |
| 6 | ENTER WAVE ANGLE α_0 , PRESS R/S | α_0 (deg) | [R/S] | HO? |
| 7 | ENTER WAVE HEIGHT H_0 , PRESS R/S | H_0 (ft.) | [R/S] | Z? |
| 8 | ENTER DEPTH BELOW SURFACE, Z, PRESS R/S | Z (ft.) | [R/S] | PHASE? |
| 9 | ENTER WAVE PHASE ANGLE θ , PRESS R/S | θ (deg) | [R/S] | |
| 10 | READ k_d (wave number * depth) | | | k_d |
| 11 | READ n (ratio of group wave speed to wave celerity) | | | n |
| 12 | READ C_g (group wave speed) | | | C_g (ft/sec) |
| 13 | READ K_s (shoaling coefficient) | | | K_s |
| 14 | READ K_r (refraction coefficient) | | | K_r |
| 15 | READ H (wave height) | | | H (ft.) |
| 16 | READ u (horizontal orbital velocity) | | | u (ft/sec) |
| 17 | READ w (vertical orbital velocity) | | | w (ft/sec) |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | note: " = [ALPHA] | | | |

101R-41CV-2

User Instructions

| | | | | SIZE: |
|------|---|-------|-------------|---------|
| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
| | TO COMPUTE IN METRIC UNITS: | | | |
| 2a | PRESS GTO "M" | | GTO "M" | |
| | STEPS 3a-17a ARE THE SAME AS | | | |
| | STEPS 3-17 EXCEPT | | | |
| | INPUT H_0, Z IN METERS | | | |
| | OUTPUT H (meters) | | | |
| | C_g, U, W IN METERS/SEC | | | |
| | EXAMPLES 1 and 1a: | | | |
| | $T = 8 \text{ sec}, d = 50 \text{ ft (15.244m)}, \alpha_0 = -30^\circ$ | | | |
| | $H_0 = 18 \text{ ft (5.4878m)}, Z = -15 \text{ ft (-4.5732m)}, \theta = 60^\circ$ | | | |
| | PRINTOUTS: | | | |
| | ENGLISH | | METRIC | |
| | PERIOD= | | PERIOD= | |
| | 8.0000 *** | | 8.0000 *** | |
| | DEPTH= | | DEPTH= | |
| | 50.0000 *** | | 15.2440 *** | |
| | AO= | | AO= | |
| | 30.0000 *** | | 30.0000 *** | |
| | HO= | | HO= | |
| | 18.0000 *** | | 5.4878 *** | |
| | Z= | | Z= | |
| | -15.0000 *** | | -4.5732 *** | |
| | PHASE= | | PHASE= | |
| | 60.0000 *** | | 60.0000 *** | |
| | KI= | | KI= | |
| | 1.1631 *** | | 1.1600 *** | |
| | H= | | H= | |
| | 0.7294 *** | | 0.7302 *** | |
| | CG= | | CG= | |
| | 24.6248 *** | | 7.5367 *** | |
| | KS= | | KS= | |
| | 0.9124 *** | | 0.9103 *** | |
| | KR= | | KR= | |
| | 0.9746 *** | | 0.9752 *** | |
| | H= | | H= | |
| | 16.0095 *** | | 4.8716 *** | |
| | U= | | U= | |
| | 2.9437 *** | | 0.9000 *** | |
| | W= | | W= | |
| | 2.4256 *** | | 1.0465 *** | |

101R-41CV-3

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|--------------|----------|--|------|------------|----------|---|
| 01 | LBL "LINEAR" | | | 56 | STO 15 | | $0 \rightarrow R_{15}$ |
| 02 | "E OR M?" | | | 57 | LBL "MAIN" | | |
| 03 | PROMPT | | | 58 | XEQ 00 | | |
| 04 | LBL E | | | 59 | 2 | | |
| 05 | 32.2 | | | 60 | * | | |
| 06 | STO 14 | | $g(\text{English}) \rightarrow R_{14}$ | 61 | STO 11 | | $4\pi d/L \rightarrow R_{11}$ |
| *07 | "ENGLISH" | | | 62 | XEQ 01 | | |
| *08 | PRA | | | 63 | 1/X | | |
| 09 | GTO 03 | | | 64 | RCL 11 | | |
| 10 | LBL "M" | | | 65 | * | | |
| *11 | "METRIC" | | | 66 | 1 | | |
| *12 | PRA | | | 67 | + | | |
| 13 | 9.81 | | | 68 | 2 | | |
| 14 | STO 14 | | $g(\text{Metric}) \rightarrow R_{14}$ | 69 | / | | |
| 15 | LBL 03 | | | *70 | "N=" | | $n \rightarrow R_x$ |
| 16 | "PERIOD?" | | | *71 | PRA | | |
| 17 | PROMPT | | | *72 | PRX | | |
| *18 | "PERIOD=" | | | 73 | STO 11 | | $n \rightarrow R_{11}$ |
| *19 | PRA | | | 74 | RCL 04 | | |
| *20 | PRX | | | 75 | * | | |
| 21 | STO 02 | | $T \rightarrow R_{02}$ | 76 | RCL 02 | | |
| 22 | "DEPTH?" | | | 77 | / | | |
| 23 | PROMPT | | | *78 | "CG=" | | $C_g \rightarrow R_x$ |
| *24 | "DEPTH=" | | | *79 | PRA | | |
| *25 | PRA | | | *80 | PRX | | |
| *26 | PRX | | | 81 | 1/X | | |
| 27 | PI | | | 82 | RCL 02 | | |
| 28 | * | | | 83 | * | | |
| 29 | 2 | | | 84 | RCL 14 | | |
| 30 | * | | | 85 | * | | |
| 31 | STO 01 | | $2\pi d \rightarrow R_{01}$ | 86 | 4 | | |
| 32 | "AO?" | | | 87 | / | | |
| 33 | PROMPT | | | 88 | PI | | |
| *34 | "AO=" | | | 89 | / | | |
| *35 | PRA | | | 90 | SQRT | | $K_s = \sqrt{C_{g0}/C_g} \rightarrow R_x$ |
| *36 | PRX | | | *91 | "KS=" | | |
| 37 | SIN | | | *92 | PRA | | |
| 38 | STO 00 | | $\sin \alpha_0 \rightarrow R_{00}$ | *93 | PRX | | |
| 39 | "HO?" | | | 94 | STO 11 | | $K_s \rightarrow R_{11}$ |
| 40 | PROMPT | | | 95 | RCL 00 | | |
| *41 | "HO=" | | | 96 | RCL 01 | | |
| *42 | PRA | | | 97 | * | | |
| *43 | PRX | | | 98 | RCL 03 | | $K_0 \sin \alpha_0$ |
| 44 | STO 08 | | $H_0 \rightarrow R_{08}$ | 99 | / | | |
| 45 | "Z?" | | | 100 | RCL 09 | | $\sin \alpha$ |
| 46 | PROMPT | | | 101 | / | | |
| *47 | "Z=" | | | 102 | X+2 | | |
| *48 | PRA | | | 103 | 1 | | |
| *49 | PRX | | | 104 | - | | |
| 50 | STO 12 | | | 105 | CHS | | $\cos^2 \alpha$ |
| 51 | "PHASE?" | | $z \rightarrow R_{12}$ | 106 | 1/X | | |
| 52 | PROMPT | | | 107 | 1 | | |
| *53 | "PHASE=" | | | 108 | ENTER+ | | |
| *54 | PRA | | | 109 | RCL 00 | | |
| *55 | PRX | | | 110 | X+2 | | |
| | | | | 111 | - | | |

*DELETE THESE LINES IF A PRINTER IS NOT AVAILABLE. 101R-41CV-4
ALSO SEE 'OPERATING LIMITS AND WARNINGS' ON PAGE 101R-41CV-1.

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------------|-----------|----------|--|------------------|-----------|----------|---------------------------------------|
| 112 * | | | | *168 *W= | | | $w \rightarrow R_x$ |
| 113 SORT | | | | *169 PRA | | | |
| 114 SORT | | | | *170 PRX | | | |
| 115 STO 10 | | | $K_r \rightarrow R_{10}$ | 171 RTN | | | |
| *116 *K= | | | $K_r \rightarrow R_x$ | 172*LBL 00 | | | *kd "subroutine" |
| *117 PRA | | | | 173 RCL 02 | | | lines 172-218 |
| *118 PRX | | | | 174 X+2 | | | |
| 119 RCL 08 | | | | 175 RCL 14 | | | |
| 120 PCL 10 | | | | 176 * | | | |
| 121 * | | | | 177 2 | | | |
| 122 RCL 11 | | | | 178 / | | | |
| 123 * | | | | 179 PI | | | |
| *124 *H= | | | $H \rightarrow R_x$ | 180 / | | | |
| *125 PRA | | | | 181 STO 03 | | | $L_0 \rightarrow R_{03}$ |
| *126 PRX | | | | 182*LBL *ITERAT* | | | |
| 127 PCL 14 | | | | 183 STO 11 | | | $L_{old} \rightarrow R_{11}$ |
| 128 * | | | | 184 1/X | | | |
| 129 PCL 02 | | | | 185 PCL 01 | | | |
| 130 * | | | | 186 * | | | |
| 131 2 | | | | 187 STO 13 | | | $\frac{2\pi d}{L} \rightarrow R_{13}$ |
| 132 / | | | | 188 XEQ 02 | | | L_{old} |
| 133 RCL 04 | | | | 189 STO 06 | | | $\cosh(R_{13}) \rightarrow R_{06}$ |
| 134 / | | | | 190 RCL 13 | | | |
| 135 PCL 06 | | | | 191 XEQ 01 | | | |
| 136 / | | | | 192 STO 05 | | | $\sinh(R_{13}) \rightarrow R_{05}$ |
| 137 STO 08 | | | $\frac{H g T}{2 L} \frac{1}{\cosh(\frac{2\pi d}{L})} \rightarrow R_{08}$ | 193 RCL 06 | | | |
| 138 PCL 01 | | | | 194 / | | | |
| 139 2 | | | | 195 PCL 03 | | | |
| 140 / | | | | 196 * | | | |
| 141 PI | | | | 197 RCL 11 | | | |
| 142 / | | | | 198 + | | | |
| 143 PCL 12 | | | | 199 2 | | | |
| 144 + | | | | 200 / | | | $L' \rightarrow R_{04}$ |
| 145 2 | | | | 201 STO 04 | | | |
| 146 * | | | | 202 PCL 11 | | | |
| 147 PI | | | | 203 - | | | |
| 148 * | | | | 204 ABS | | | |
| 149 RCL 04 | | | | 205 1 | | | |
| 150 / | | | | 206 XYY? | | | |
| 151 STO 05 | | | $\frac{2\pi(z+d)}{L} \rightarrow R_{05}$ | 207 GTO 25 | | | |
| 152 XEQ 02 | | | | 208 RCL 04 | | | |
| 153 RCL 08 | | | | 209 GTO *ITERAT* | | | |
| 154 * | | | | 210*LBL 25 | | | |
| 155 RCL 15 | | | | 211 RCL 01 | | | |
| 156 COS | | | | 212 RCL 04 | | | |
| 157 * | | | $u \rightarrow R_x$ | 213 / | | | |
| *158 *U= | | | | 214 STO 09 | | | $kd \rightarrow R_{09}$ |
| *159 PRA | | | | *215 *KD= | | | $kd \rightarrow R_x$ |
| *160 PRX | | | | *216 PRA | | | |
| 161 RCL 05 | | | | *217 PRX | | | |
| 162 XEQ 01 | | | | 218 RTN | | | |
| 163 RCL 09 | | | | 219*LBL 01 | | | subroutine |
| 164 * | | | | 220 STO 07 | | | $\sinh(\)$ lines |
| 165 PCL 15 | | | | 221 F+X | | | 219-228 |
| 166 SIN | | | | 222 RCL 07 | | | |
| 167 * | | | | 223 CHS | | | |

* DELETE THESE LINES IF A PRINTER IS NOT AVAILABLE. 101R-41CV-5
ALSO SEE 'OPERATING LIMITS AND WARNINGS' ON PAGE 101R-41CV-1.

Program Listing

[illegible]

*DELETE THESE LINES IF A PRINTER IS NOT AVAILABLE. 101R-41CV-6
ALSO SEE 'OPERATING LIMITS AND WARNINGS' ON PAGE 101R-41CV-1.

Program Description

| | | | |
|----------------------|---|-----------------|----------|
| Program Title | 102R-41CV Linear Wave Approximation to Breaking Wave Height and Breaking Wave Angle (RPN Logic) | | |
| Name | T.L. Walton, Jr. | Date | 1/82 |
| Address | Coastal Engineering Research Center | | |
| City | Kingman Building Fort Belvoir, | State | Virginia |
| | | Zip Code | 22060 |

Program Description, Equations, Variables, etc.

This program calculates breaking wave height, H_b , and breaking wave angle, α_b , using linear wave theory approximations combined with the shallow-water breaking assumption. Input parameters are wave height, H , wave period, T , wave angle, α , and the water depth, d , where the preceding three variables are measured. An additional input parameter is nearshore beach slope, m . The ratio of the breaking wave height to the water depth at breaking is predicted using the equation

$$\kappa = H_b/d_b = 1.16 \left(\frac{m}{\sqrt{H'_0}/L_0} \right)^{0.22}$$

from Singamsetti and Wind (1980), where d_b is the water depth at breaking, H'_0 the deepwater wave height, and L_0 the deepwater wavelength. This solution requires the assumption of straight and parallel offshore bottom contours for the application of Snell's law of refraction. Input wave parameters H , T , and α can be in any depth of water, d . Algorithm uses English or metric system of units. The development of the equation is derived on the attached solution sheet.

REFERENCES

SINGAMSETTI, S.R., and WIND, H.G., "Characteristics of Shoaling and Breaking Periodic Waves Normally Incident to Plane Beaches of Constant Slope," Report No. M1371, Toegepast Onderzoek Waterstaat, July 1980.

U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, *Shore Protection Manual*, 3d ed., Vol. I, Ch. 2, Stock No. 008-022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977.

Operating Limits and Warnings

102R-41CV-1

Development of the equation:

From conservations of energy

$$\frac{\gamma H^2}{8} C_g \cos \alpha = \frac{\gamma H_i^2}{8} C_{gi} \cos \alpha_i \quad (1)$$

where the subscript i indicates incident wave parameters.

If left-hand side of above equation represents conditions at breaking then

$$C_g = C = C_b = \sqrt{gd_b} = \sqrt{gH_b/\kappa} \quad (2)$$

where
$$\kappa = \frac{H_b}{d_b} \quad (3)$$

Now assume
$$\kappa = 1.16 \left(\frac{m}{\sqrt{H_0^1/L_0}} \right)^{0.22} \quad (4)$$

where H_0^1 is unrefracted deepwater wave height.

Using (1), (2), (3), and (4) it can be found

$$H_b = \left\{ \left(\frac{\kappa}{g} \right)^{1/2} H_i^2 C_{gi} \cos \alpha_i \right\}^{2/5} \quad (5)$$

From Snell's law of refraction

$$\frac{\sin \alpha_b}{C_b} = \frac{\sin \alpha_i}{C_i} \quad (6)$$

therefore,

$$\sin \alpha_b = \left(\frac{\sin \alpha_i}{C_i} \right) \left(\frac{g}{\kappa} H_b \right)^{1/2} \quad (7)$$

User Instructions

102R-41CV LINEAR APPROXIMATION TO BREAKING
WAVE HEIGHT AND BREAKING WAVE ANGLE (RPN LOGIC)

SIZE: 021

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|------|--|-----------------|----------------|-------------------|
| 1 | LOAD PROGRAM (ANGLE B) | | [XEQ] "ANGLEB" | FORM? |
| | | | | |
| | TO CALCULATE H_b, α_b IN ENGLISH UNITS: | | | |
| 2 | PRESS GTO "E" | | GTO "E" | |
| 3 | PRESS R/S | | [R/S] | SLOPE? |
| 4 | ENTER SLOPE m , PRESS R/S | m | [R/S] | DEPTH? |
| 5 | ENTER DEPTH D , PRESS R/S | d (ft.) | [R/S] | ANGLE? |
| 6 | ENTER ANGLE α , PRESS R/S | α (deg.) | [R/S] | H ? |
| 7 | ENTER WAVE HEIGHT, H , PRESS R/S | H (ft.) | [R/S] | PERIOD? |
| 8 | ENTER WAVE PERIOD T , PRESS R/S | T (sec) | [R/S] | |
| 9 | READ K_d | | | K_d |
| 10 | PRESS R/S, READ n | | [R/S] | n |
| 11 | PRESS R/S, READ C_g | | [R/S] | C_g (ft/sec) |
| 12 | PRESS R/S, READ K_s | | [R/S] | K_s |
| 13 | PRESS R/S, READ $H_0' = H_0 K_r$ | | [R/S] | H_0' (ft.) |
| 14 | PRESS R/S, READ H_b | | [R/S] | H_b (ft.) |
| 15 | PRESS R/S, READ α_b | | [R/S] | α_b (deg.) |
| | | | | |
| | TO CALCULATE H_b, α_b IN METRIC UNITS: | | | |
| | FOLLOW THE SAME INSTRUCTIONS AS ABOVE EXCEPT: | | | |
| | PRESS GTO "M" AT STEP 20. | | | |
| | INPUT D and H IN METERS. | | | |
| | C_g, H_0', H_b ARE OUTPUT IN $M/S, m, m$ RESPECTIVELY. | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | note: " = [ALPHA] | | | |

102R-41CV-3

User Instructions

| | | | SIZE: | |
|------|---|-------------------------|------------------|---------|
| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
| | EXAMPLE : | | | |
| | Input $m = 0.10$, $d = 50 \text{ ft } (15.24 \text{ m})$ | | | |
| | $\alpha = 30^\circ$, $H = 18 \text{ ft } (5.4878 \text{ m})$ | | | |
| | $T = 8 \text{ sec}$. | | | |
| | ENGLISH PRINTOUT: | METRIC PRINTOUT: | | |
| | ENGLISH SLOPE= | _____ | METRIC SLOPE= | _____ |
| | 0.1000 *** | _____ | 0.1000 *** | _____ |
| | DEPTH= | _____ | DEPTH= | _____ |
| | 50.0000 *** | _____ | 15.2439 *** | _____ |
| | ANGLE= | _____ | ANGLE= | _____ |
| | 30.0000 *** | _____ | 30.0000 *** | _____ |
| | H= | _____ | H= | _____ |
| | 18.0000 *** | _____ | 5.4878 *** | _____ |
| | PERIOD= | _____ | PERIOD= | _____ |
| | 8.0000 *** | _____ | 8.0000 *** | _____ |
| | KD= | _____ | KD= | _____ |
| | 1.1631 *** | _____ | 1.1600 *** | _____ |
| | N= | _____ | N= | _____ |
| | 0.7294 *** | _____ | 0.7302 *** | _____ |
| | CG= | _____ | CG= | _____ |
| | 24.6240 *** | _____ | 7.5367 *** | _____ |
| | KS= | _____ | KS= | _____ |
| | 0.9124 *** | _____ | 0.9107 *** | _____ |
| | HOKP= | _____ | HOKP= | _____ |
| | 19.7284 *** | _____ | 6.0286 *** | _____ |
| | HB= | _____ | HB= | _____ |
| | 16.9087 *** | _____ | 5.1855 *** | _____ |
| | AB= | _____ | AB= | _____ |
| | 20.7859 *** | _____ | 20.7406 *** | _____ |

102R-41CV-4

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|---------------|----------|--|------|---------------|----------|---|
| 01 | *LBL "ANGLE?" | | | 57 | / | | |
| 02 | *E OR M ? | | | 58 | STO 03 | | $L_0 \rightarrow R_{03}$ |
| 03 | PROMPT | | | 59 | *LBL "ITERAT" | | |
| 04 | *LBL E | | | 60 | STO 11 | | $L_{old} \rightarrow R_{11}$ |
| 05 | 32.3 | | | 61 | 1/X | | |
| 06 | STO 14 | | | 62 | RCL 12 | | |
| *07 | *ENGLISH* | | $g(\text{English}) \rightarrow R_{14}$ | 63 | * | | |
| *08 | PRR | | | 64 | STO 13 | | $\frac{2\pi d}{L_{old}} \rightarrow R_{13}$ |
| 09 | GTO 01 | | | 65 | XEQ 02 | | $\cosh(R_{13}) \rightarrow R_{06}$ |
| 10 | *LBL "M" | | | 66 | STO 06 | | |
| *11 | *METRIC* | | | 67 | RCL 13 | | |
| *12 | PRR | | | 68 | XEQ 03 | | |
| 13 | 9.81 | | | 69 | STO 05 | | $\sinh(R_{13}) \rightarrow R_{05}$ |
| 14 | STO 14 | | $g(\text{Metric}) \rightarrow R_{14}$ | 70 | RCL 06 | | |
| 15 | *LBL 01 | | | 71 | / | | |
| *16 | *SLOPE=* | | | 72 | RCL 03 | | |
| *17 | PRR | | | 73 | * | | |
| 18 | *SLOPE?* | | | 74 | RCL 11 | | |
| 19 | PROMPT | | | 75 | + | | |
| *20 | PRX | | | 76 | 2 | | |
| 21 | STO 15 | | $m \rightarrow R_{15}$ | 77 | / | | |
| *22 | *DEPTH=* | | | 78 | STO 04 | | |
| *23 | PRR | | | 79 | RCL 11 | | |
| 24 | *DEPTH?* | | | 80 | - | | |
| 25 | PROMPT | | | 81 | ABS | | |
| *26 | PRX | | | 82 | 1 | | |
| 27 | STO 01 | | $d \rightarrow R_{01}$ | 83 | X/Y? | | |
| 28 | P1 | | | 84 | GTO 13 | | |
| 29 | * | | | 85 | RCL 04 | | |
| 30 | 2 | | | 86 | GTO "ITERAT" | | |
| 31 | * | | | 87 | *LBL 13 | | |
| 32 | STO 12 | | $2\pi d \rightarrow R_{12}$ | 88 | RCL 12 | | |
| *33 | *ANGLE=* | | | 89 | RCL 04 | | |
| *34 | PRR | | | 90 | / | | |
| 35 | *ANGLE?* | | | 91 | STO 09 | | $k_d \rightarrow R_{09}$ |
| 36 | PROMPT | | | *92 | *KD=* | | $\rightarrow \text{display}$ |
| *37 | PRX | | | *93 | PRR | | |
| 38 | STO 00 | | | *94 | PRX | | |
| *39 | *H=* | | | 95 | STOP | | |
| *40 | PRR | | | 96 | 2 | | |
| 41 | *H?* | | | 97 | * | | |
| 42 | PROMPT | | | 98 | STO 11 | | $2k_d \rightarrow R_{11}$ |
| *43 | PRX | | | 99 | XEQ 03 | | |
| 44 | STO 08 | | $H \rightarrow R_{08}$ | 100 | 1/X | | |
| *45 | *PERIOD=* | | | 101 | RCL 11 | | |
| *46 | PRR | | | 102 | * | | |
| 47 | *PERIOD?* | | | 103 | 1 | | |
| 48 | PROMPT | | | 104 | + | | |
| *49 | PRX | | | 105 | 2 | | |
| 50 | STO 02 | | $T \rightarrow R_{02}$ | 106 | / | | |
| 51 | Y? | | | 107 | STO 01 | | $n \rightarrow R_{01}$ |
| 52 | RCL 14 | | | *108 | *N=* | | $\rightarrow \text{display}$ |
| 53 | * | | | *109 | PRR | | |
| 54 | 2 | | | *110 | PRX | | |
| 55 | / | | | 111 | STOP | | |
| 56 | P1 | | | 112 | RCL 04 | | |

*DELETE THESE STEPS IF A PRINTER IS NOT AVAILABLE. 102R-41CV-5

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|-------------|-----------|----------|--------------------------|-------------|-----------|----------|-----------------------|
| 113 * | | | | *169 *HB= | | | H_b in display |
| 114 RCL 02 | | | | *170 PRA | | | |
| 115 / | | | | *171 PRX | | | |
| 116 STO 04 | | | $C_g \rightarrow R_{04}$ | 172 STOP | | | |
| *117 *CG= | | | $\rightarrow display$ | 173 RCL 06 | | | |
| *118 PRA | | | | 174 1/X | | | |
| *119 PRX | | | | 175 * | | | |
| 120 STOP | | | | 176 SQRT | | | |
| 121 1/X | | | | 177 RCL 00 | | | |
| 122 RCL 02 | | | | 178 SIN | | | |
| 123 * | | | | 179 * | | | |
| 124 RCL 14 | | | | 180 RCL 04 | | | |
| 125 * | | | | 181 / | | | |
| 126 4 | | | | 182 RCL 01 | | | |
| 127 / | | | | 183 * | | | |
| 128 PI | | | | 184 ASIN | | | |
| 129 / | | | | *185 *AB= | | | α_b in display |
| 130 SQRT | | | | *186 PRA | | | |
| 131 STO 11 | | | $K_s \rightarrow R_{11}$ | *187 PRX | | | |
| *132 *KS= | | | $\rightarrow display$ | 188 STOP | | | |
| *133 PRA | | | | 189 ATN | | | $\sinh()$ subroutine |
| *134 PRX | | | | 190 *LBL 03 | | | |
| 135 STOP | | | | 191 STO 07 | | | |
| 136 RCL 00 | | | | 192 E+X | | | |
| 137 RCL 11 | | | H_0' in display | 193 RCL 07 | | | |
| 138 / | | | | 194 CHS | | | |
| *139 *HOKR= | | | | 195 E+X | | | |
| *140 PRA | | | | 196 - | | | |
| *141 PRX | | | | 197 2 | | | |
| 142 STOP | | | | 198 / | | | |
| 143 RCL 03 | | | | 199 RTN | | | |
| 144 / | | | | 200 *LBL 02 | | | $\cosh()$ subroutine |
| 145 SQRT | | | | 201 STO 07 | | | |
| 146 RCL 15 | | | | 202 E+X | | | |
| 147 / | | | | 203 RCL 07 | | | |
| 148 1/X | | | | 204 CHS | | | |
| 149 .22 | | | | 205 E+X | | | |
| 150 Y+X | | | | 206 + | | | |
| 151 1.16 | | | | 207 2 | | | |
| 152 * | | | | 208 / | | | |
| 153 RCL 14 | | | | 209 .END. | | | |
| 154 / | | | | | | | |
| 155 STO 06 | | | | | | | |
| 156 RCL 00 | | | | | | | |
| 157 X+2 | | | | | | | |
| 158 RCL 04 | | | | | | | |
| 159 * | | | | | | | |
| 160 RCL 00 | | | | | | | |
| 161 COS | | | | | | | |
| 162 * | | | | | | | |
| 163 .4 | | | | | | | |
| 164 Y+X | | | | | | | |
| 165 RCL 06 | | | | | | | |
| 166 .2 | | | | | | | |
| 167 Y+X | | | | | | | |
| 168 * | | | | | | | |

* DELETE THESE STEPS IF A PRINTER IS NOT AVAILABLE.

102R-41CV-6

Program Description

| | | | | | |
|--|---|-------|----------|----------|-------|
| Program Title | 103R-41C Shallow-Water Wave Forecasting Equations (RPN Logic) | | | | |
| Name | T.L. Walton, Jr. | | Date | 1/82 | |
| Address | Coastal Engineering Research Center | | | | |
| | Kingman Building | | | | |
| City | Fort Belvoir, | State | Virginia | Zip Code | 22060 |
| Program Description, Equations, Variables, etc. | | | | | |
| <p>This algorithm computes the wave height, H, wave period, T, and minimum duration, t, from input values of the water depth, d, fetch length, F, and adjusted windspeed, U_A, using equations (1), (2), and (3) of CETN-I-6. Equations (1) and (2) are for constant water depth and unlimited wind duration and have been revised from equations (3-25) and (3-26) of the Shore Protection Manual. Wave height and period in this algorithm are significant wave height and period. Algorithm uses English or metric system of units.</p> | | | | | |
| REFERENCES | | | | | |
| <p>U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, <i>Shore Protection Manual</i>, 3d ed., Vols. I, II, and III, Stock No. 008-022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977, 1,262 pp.</p> | | | | | |
| <p>U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, "Method for Determining Adjusted Windspeed, U_A, for Wave Forecasting," CETN-I-5, Fort Belvoir, Va., 1981.</p> | | | | | |
| <p>U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, "Revised Method for Wave Forecasting in Shallow Water," CETN-I-6, Fort Belvoir, Va., 1981.</p> | | | | | |
| <p>U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, "Revised Method for Wave Forecasting in Deep Water," CETN-I-7, Fort Belvoir, Va., 1981.</p> | | | | | |
| Operating Limits and Warnings | | | | | |
| <p>If a printer is not used, R/S must be inserted where output values are desired (i.e., where printer output steps are deleted).</p> | | | | | |

103R-41CV-1

User Instructions

103R-41CV SHALLOW WATER WAVE FORECASTING EQUATIONS (RPN LOGIC)

SIZE: 021

[illegible]

103R-41CV-2

User Instructions

| | | | SIZE: | |
|------|--|------------------------|----------|---------|
| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
| | EXAMPLES 1 and 1a | | | |
| | 1. ENGLISH UNITS, USING | | | |
| | $V_A = 40 \text{ mph}$, $F = 300 \text{ miles}$ | | | |
| | $d = 20 \text{ ft.}$ | | | |
| | 1a. METRIC UNITS, USING | | | |
| | $V_A = 64.416 \text{ km/hr}$, $F = 483.12 \text{ km}$ | | | |
| | $d = 6.1 \text{ m}$ | | | |
| | | | | |
| | PRINTOUTS | | | |
| | ENGLISH UNITS: | METRIC UNITS: | | |
| | ENGLISH | METRIC | | |
| | WQ= | WQ= | | |
| | 40.0000 *** | 64.4160 *** | | |
| | FETCH= | FETCH= | | |
| | 300.0000 *** | 483.1200 *** | | |
| | DEPTH= | DEPTH= | | |
| | 20.0000 *** | 6.1000 *** | | |
| | H= | H= | | |
| | 4.5717 ft. *** | 1.3809 m. *** | | |
| | T= | T= | | |
| | 5.6032 sec. *** | 5.6032 sec. *** | | |
| | TIME= | TIME= | | |
| | 3.7253 hrs. *** | 3.7307 hrs. *** | | |

103R-41CV-3

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|--------------|----------|--|------|-----------|----------|--|
| 01 | LBL "FOURST" | | | 57 | RCL 05 | | |
| 02 | "E OR M ?" | | | 58 | * | | |
| 03 | PROMPT | | | 59 | STO 01 | | $g/U_A^2 \rightarrow R_{01}$ |
| 04 | LBL E | | | 60 | RCL 00 | | |
| 05 | 32.2 | | $g(\text{English}) \rightarrow R_{09}$ | 61 | .75 | | |
| 06 | STO 09 | | English Conversion | 62 | Y+X | | |
| 07 | 1.47 | | $\rightarrow R_{07}$ | 63 | .53 | | |
| 08 | STO 07 | | English Conversion | 64 | * | | |
| 09 | 5200 | | $\rightarrow R_{01}$ | 65 | XEQ 03 | | |
| 10 | STO 01 | | | 66 | STO 04 | | $\tanh[.53(\frac{gd}{U_A^2})^{0.75}]$ |
| *11 | "ENGLISH" | | | 67 | RCL 01 | | $\rightarrow R_{09}$ |
| *12 | PRR | | | 68 | SQRT | | |
| 13 | GTO 01 | | | 69 | .00565 | | |
| 14 | LBL "M" | | | 70 | * | | |
| *15 | "METRIC" | | | 71 | RCL 04 | | |
| *16 | PRR | | | 72 | / | | |
| 17 | 9.81 | | $g(\text{Metric}) \rightarrow R_{09}$ | 73 | XEQ 03 | | |
| 18 | STO 09 | | metric conversion | 74 | RCL 04 | | $\tanh[\frac{.00565(gF)}{R_{09}}(\frac{gF}{U_A^2})^{0.5}]$ |
| 19 | .2778 | | $\rightarrow R_{09}$ | 75 | * | | |
| 20 | STO 07 | | metric conversion | 76 | .283 | | |
| 21 | .0000 | | $\rightarrow R_{01}$ | 77 | * | | |
| 22 | STO 01 | | | 78 | RCL 00 | | |
| 23 | LBL 01 | | | 79 | / | | |
| 24 | "U?" | | | *80 | "H=" | | |
| 25 | PROMPT | | | *81 | PRR | | |
| *26 | "U=" | | | *82 | PRX | | |
| *27 | PRR | | | 83 | RCL 00 | | |
| *28 | PRX | | $U_A \rightarrow R_{03}$ | 84 | .375 | | |
| 29 | STO 03 | | | 85 | Y+X | | |
| 30 | "FETCH?" | | | 86 | .833 | | |
| 31 | PROMPT | | | 87 | * | | |
| *32 | "FETCH=" | | | 88 | XEQ 03 | | $\tanh[0.833(\frac{gd}{U_A^2})^{0.375}]$ |
| *33 | PRR | | | 89 | STO 04 | | |
| *34 | PRX | | | 90 | RCL 01 | | $\rightarrow R_{09}$ |
| 35 | STO 05 | | $F \rightarrow R_{05}$ | 91 | .333 | | |
| 36 | "DEPTH?" | | | 92 | Y+X | | |
| 37 | PROMPT | | | 93 | .0379 | | |
| *38 | "DEPTH=" | | | 94 | * | | |
| *39 | PRR | | | 95 | RCL 04 | | |
| *40 | PRX | | | 96 | / | | |
| 41 | STO 06 | | $d \rightarrow R_{06}$ | 97 | XEQ 03 | | $\tanh[\frac{0.0379(gF)}{R_{09}}(\frac{gF}{U_A^2})^{0.333}]$ |
| 42 | RCL 03 | | | 98 | RCL 04 | | |
| 43 | RCL 07 | | | 99 | * | | |
| 44 | * | | | 100 | 7.54 | | |
| 45 | STO 07 | | converted $U_A \rightarrow R_{07}$ | 101 | * | | |
| 46 | RCL 09 | | | 102 | RCL 00 | | |
| 47 | RCL 07 | | | 103 | / | | |
| 48 | X+2 | | | 104 | RCL 07 | | |
| 49 | / | | | 105 | / | | |
| 50 | STO 02 | | $g/U_A^2 \rightarrow R_{08}$ | *106 | "T=" | | |
| 51 | RCL 06 | | | *107 | PRR | | |
| 52 | * | | | *108 | PRX | | |
| 53 | STO 00 | | $gd/U_A^2 \rightarrow R_{00}$ | 109 | RCL 09 | | |
| 54 | RCL 00 | | | 110 | * | | |
| 55 | RCL 01 | | | 111 | RCL 07 | | |
| 56 | * | | | 112 | . | | |

103R-41CV-4

*DELETE IF PRINTER IS NOT AVAILABLE
ALSO SEE 'operating Limits and Warnings' on p. 103R-41CV-1

Program Listing

[illegible]

103R-41CV-5

* DELETE IF PRINTER IS NOT AVAILABLE.
ALSO SEE 'Operating Limits and Warnings' ON P. 103R-41CV-1.

Program Description

| | | | |
|----------------------|--|-----------------|----------|
| Program Title | 104R-41CV Depth-Limited Design Breaking Wave Height at Structure (RPN Logic) | | |
| Name | T.L. Walton, Jr. | Date | 1/82 |
| Address | Coastal Engineering Research Center | | |
| City | Kingman Building | State | Virginia |
| | Fort Belvoir, | Zip Code | 22060 |

Program Description, Equations, Variables, etc.

This algorithm computes the depth-limited breaking wave height at a structure for design purposes. It can be used in lieu of Figure 7-4 of the Shore Protection Manual. The equation for the curves in Figure 7-4 is not given in the SPM but can be found by simultaneous solution of SPM equations (2-91), (2-92), (2-93), (7-3), and (7-4). Input is wave period, T , and water depth at the structure toe, d_s . The development of the equation is derived on the attached solution sheet. Algorithm uses English or metric system of units.

REFERENCE

U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, *Shore Protection Manual*, 3d ed., Vols. I and II, Chs. 2 and 7, Stock No. 008-022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977.

Operating Limits and Warnings

104R-41CV-1

The following equations are given in the Shore Protection Manual:

$$\frac{d_b}{H_b} = \frac{1}{b - (aH_b/gT^2)} \quad (2-91)$$

$$a = 43.75(1 - e^{-1.9m}) \quad (2-92)$$

$$b = \frac{1.56}{(1 + e^{-19.5m})} \quad (2-93)$$

$$x_p = \tau_p H_b = (4.0 - 9.25 m) H_b \quad (7-3)$$

$$H_b = \frac{d_s}{\beta - m\tau_p} \quad (7-4)$$

Equation (7-4) can be rewritten in dimensionless form as:

$$\hat{H}_b = \frac{\hat{d}_s}{[(b - a\hat{H}_b)^{-1} - m\tau_p]}$$

where

$$\hat{H}_b = H_b/gT^2 \text{ and } \hat{d}_s = d_s/gT^2$$

The above equation can then be solved via the quadratic formula for \hat{H}_b in terms of \hat{d}_s , τ_p , m , a , and b where the positive root provides useful results.

$$\hat{H}_b = \left\{ (m\tau_p b - a\hat{d}_s - 1) + \left[(m\tau_p b - a\hat{d}_s - 1)^2 + 4am\tau_p b \hat{d}_s \right]^{1/2} \right\} (2am\tau_p)^{-1}$$

This is the equation used in the program for design breaking wave height.

User Instructions

104R-41CV DEPTH-LIMITED DESIGN BREAKING
WAVE HEIGHT AT STRUCTURE (RPN LOGIC)

SIZE: 021

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|------|--|--------------------|------------------|----------------------|
| 1 | LOAD PROGRAM (HB) | | [XEQ] "HB" | E OR M? |
| | | | | |
| | TO CALCULATE H_b IN ENGLISH UNITS: | | | |
| 2 | PRESS GTO "E" | | GTO "E" | |
| 3 | PRESS R/S | | [R/S] | SLOPE? |
| 4 | ENTER SLOPE m , PRESS R/S | m | [R/S] | DEPTH? |
| 5 | ENTER DEPTH D , PRESS R/S | $d(\text{ft})$ | [R/S] | PERIOD? |
| 6 | ENTER PERIOD T , PRESS R/S | $T(\text{sec})$ | [R/S] | |
| 7 | READ H_b IN FEET | | | $H_b(\text{ft})$ |
| | | | | |
| | TO CALCULATE H_b IN METRIC UNITS: | | | |
| 2a | PRESS GTO "M" | | GTO "M" | |
| 3a | PRESS R/S | | [R/S] | SLOPE? |
| 4a | ENTER SLOPE m , PRESS R/S | m | [R/S] | DEPTH? |
| 5a | ENTER DEPTH D , PRESS R/S | $d(\text{meters})$ | [R/S] | PERIOD? |
| 6a | ENTER PERIOD T , PRESS R/S | $T(\text{sec})$ | [R/S] | |
| 7a | READ H_b IN METERS | | | $H_b(\text{meters})$ |
| | | | | |
| | Example 1 and 1a | | | |
| | $m = 0.10$, $d = 10\text{ft}$ (3.05m), $T = 10\text{sec}$ | | | |
| | ENGLISH PRINTOUT: METRIC PRINTOUT: | | | |
| | ENGLISH | | METRIC | |
| | SLOPE= | | SLOPE= | |
| | 0.1000 *** | | 0.1000 *** | |
| | DEPTH= | | DEPTH= | |
| | 10.0000 *** | | 3.0500 *** | |
| | PERIOD= | | PERIOD= | |
| | 10.0000 *** | | 10.0000 *** | |
| | H _b = | | H _b = | |
| | 17.9810 *** | | 5.4631 *** | |
| | | | | |
| | | | | note: " = [ALPHA] |

104R-41CV-3

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|------------|----------|--|------|-----------|----------|------------------------|
| 01 | LBL "H8" | | | 57 | 1 | | |
| 02 | "E OR M ?" | | | 58 | + | | |
| 03 | PROMPT | | | 59 | 1.56 | | |
| 04 | LBL E | | | 60 | / | | |
| 05 | 32.2 | | | 61 | 1/X | | |
| 06 | STO 08 | | $g(\text{English}) \rightarrow R_{08}$ | 62 | STO 04 | | |
| *07 | "ENGLISH" | | | 63 | RCL 00 | | |
| *08 | PRA | | | 64 | ENTER↑ | | |
| 09 | GTO 01 | | | 65 | 9.25 | | |
| 10 | LBL "M" | | | 66 | + | | |
| *11 | "METRIC" | | | 67 | 4 | | |
| *12 | PRA | | | 68 | - | | |
| 13 | 9.81 | | | 69 | CHS | | |
| 14 | STO 08 | | $g(\text{Metric}) \rightarrow R_{08}$ | 70 | RCL 00 | | |
| 15 | LBL 01 | | | 71 | * | | |
| *16 | "SLOPE=" | | | 72 | STO 05 | | $m_j p = m(4 - 9.25m)$ |
| *17 | PRA | | | 73 | RCL 04 | | $\rightarrow R_{05}$ |
| 18 | "SLOPE?" | | | 74 | * | | |
| 19 | PROMPT | | | 75 | 1 | | |
| *20 | PRX | | | 76 | - | | |
| 21 | STO 00 | | $m \rightarrow R_{00}$ | 77 | RCL 01 | | |
| *22 | "DEPTH=" | | | 78 | RCL 03 | | |
| *23 | PRA | | | 79 | * | | |
| 24 | "DEPTH?" | | | 80 | - | | |
| 25 | PROMPT | | | 81 | STO 06 | | $m_j p b - a d_s - 1$ |
| *26 | PRX | | | 82 | X↑2 | | $\rightarrow R_{06}$ |
| 27 | STO 07 | | | 83 | 4 | | |
| *28 | "PERIOD=" | | | 84 | RCL 03 | | |
| *29 | PRA | | | 85 | * | | |
| 30 | "PERIOD?" | | | 86 | RCL 04 | | |
| 31 | PROMPT | | | 87 | * | | |
| *32 | PRX | | | 88 | RCL 05 | | |
| 33 | STO 09 | | $T \rightarrow R_{09}$ | 89 | * | | |
| 34 | X↑2 | | | 90 | RCL 01 | | |
| 35 | RCL 08 | | | 91 | * | | |
| 36 | * | | | 92 | + | | |
| 37 | 1/X | | | 93 | SART | | |
| 38 | RCL 07 | | | 94 | RCL 06 | | |
| 39 | * | | | 95 | + | | |
| 40 | STO 01 | | | 96 | 2 | | |
| 41 | RCL 00 | | $\frac{d_s}{gT^2} \rightarrow R_{01}$ | 97 | / | | |
| 42 | 19 | | | 98 | RCL 03 | | |
| 43 | * | | | 99 | / | | |
| 44 | CHS | | | 100 | RCL 05 | | |
| 45 | E↑X | | | 101 | / | | |
| 46 | CHS | | | 102 | RCL 01 | | |
| 47 | 1 | | | 103 | / | | |
| 48 | + | | | 104 | RCL 07 | | |
| 49 | 43.75 | | | 105 | * | | |
| 50 | * | | | *106 | "H8=" | | H_b in display |
| 51 | STO 07 | | $43.75(1 - e^{-19m}) \rightarrow R_{03}$ | *107 | PRA | | |
| 52 | RCL 00 | | | *108 | PRX | | |
| 53 | 9.5 | | | 109 | STOP | | |
| 54 | * | | | 110 | END | | |
| 55 | CHS | | | | | | |
| 56 | E↑X | | | | | | |

* THESE STEPS MUST BE DELETED IF NO PRINTER IS AVAILABLE 101R-41CV-4

Program Description

| | | | |
|----------------------|---|-----------------|----------|
| Program Title | 105R-41CV Wave Transmission - Fuchs' Equation (RPN Logic) | | |
| Name | T.L. Walton, Jr. | Date | 1/82 |
| Address | Coastal Engineering Research Center | | |
| City | Kingman Building | State | Virginia |
| | Fort Belvoir, | Zip Code | 22060 |

Program Description, Equations, Variables, etc.

This algorithm computes wavelength, L , in water depth, d , given the wave period, T . The program then computes wave transmission over a thin vertical barrier in water depth, d , using Fuchs' equation:

$$\frac{H_t}{H_i} = \sqrt{1 - \frac{\frac{4\pi h}{L} + \sinh \frac{4\pi h}{L}}{\frac{4\pi d}{L} + \sinh \frac{4\pi d}{L}}}$$

where H_t is the transmitted wave height, H_i the incident wave height, and h the height of barrier. Note that this equation *cannot* be used when wave transmission is by overtopping of a structure. Algorithm uses English or metric system of units.

REFERENCE

U.S. ARMY, CORPS OF ENGINEERS, COASTAL ENGINEERING RESEARCH CENTER, *Shore Protection Manual*, 3d ed., Vol. II, Ch. 7, Stock No. 008-022-00113-1, U.S. Government Printing Office, Washington, D.C., 1977, p. 7-62.

Operating Limits and Warnings

105R-41CV-1

User Instructions

105R-41CV WAVE TRANSMISSION - FUCHS' EQUATION (RPN logic)

SIZE: 021

| STEP | INSTRUCTIONS | INPUT | FUNCTION | DISPLAY |
|------|--|---------|---------------------|---------|
| 1 | LOAD PROGRAM (FUCH) | | [XEQ] "FUCH" | |
| | | | | |
| | TO CALCULATE IN ENGLISH UNITS: | | | |
| 2 | PRESS GTO "E" | | GTO "E" | |
| 3 | PRESS R/S | | [R/S] | DEPTH? |
| 4 | ENTER DEPTH D, PRESS R/S | d (ft.) | [R/S] | SIL HT? |
| 5 | ENTER SILL HEIGHT H, PRESS R/S | h (ft.) | [R/S] | PERIOD? |
| 6 | ENTER PERIOD T, PRESS R/S | T (sec) | [R/S] | |
| 7 | READ $K_t = H_t/H_c$ (TRANSMISSION COEFFICIENT) | | | K_t |
| | | | | |
| | TO CALCULATE IN METRIC UNITS: | | | |
| 2a | PRESS GTO "M" | | GTO "M" | |
| | STEPS 3a-7a ARE THE SAME AS STEPS 3-7 ABOVE EXCEPT | | | |
| | INPUT d, h, IN METERS | | | |
| | OUTPUT L (PRINTER ONLY) METERS | | | |
| | | | | |
| | Example 1 and 1a: | | | |
| | Values used: d=15ft (4.5732m), h=10ft (3.0488m), T=10sec | | | |
| | PRINTOUTS: | | | |
| | ENGLISH | | METRIC | |
| | DEPTH= 15.0000 *** | | DEPTH= 4.5732 *** | |
| | SIL HT= 10.0000 *** | | SIL HT= 3.0488 *** | |
| | PERIOD= 10.0000 *** | | PERIOD= 10.0000 *** | |
| | L= 213.0238 *** | | L= 64.9450 *** | |
| | KT= 0.5977 *** | | KT= 0.5977 *** | |
| | note: " = [ALPHA] | | | |

105R-41CV-2

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|--------------|----------|---|------|--------------|----------|---|
| 01 | LBL "FUCH" | | | 57 | END | | |
| 02 | "E OP M ?" | | | 58 | PCL 04 | | |
| 03 | PROMPT | | | 59 | CHS | | |
| 04 | LBL E | | | 60 | END | | |
| 05 | 32.0 | | | 61 | + | | |
| 06 | STO 06 | | $g(\text{English}) \rightarrow R_{06}$ | 62 | / | | |
| *07 | "ENGLISH" | | | 63 | RCL 01 | | $\tanh\left(\frac{2\pi d}{L_{old}}\right)$ |
| *08 | PRA | | | 64 | * | | |
| 09 | GTO 01 | | | 65 | RCL 03 | | |
| 10 | LBL "M" | | | 66 | + | | |
| *11 | "METRIC" | | | 67 | 2 | | |
| *12 | PRA | | | 68 | / | | $L' \rightarrow R_{02}$ |
| 13 | 9.01 | | | 69 | STO 02 | | |
| 14 | STO 06 | | $g(\text{Metric}) \rightarrow R_{06}$ | 70 | RCL 03 | | |
| 15 | LBL 01 | | | 71 | - | | |
| 16 | "DEPTH?" | | | 72 | ABS | | |
| 17 | PROMPT | | | 73 | 1 | | |
| *18 | "DEPTH=" | | | 74 | X?Y? | | |
| *19 | PRA | | | 75 | GTO 13 | | |
| *20 | PRX | | | 76 | RCL 02 | | |
| 21 | 2 | | | 77 | GTO "ITERAT" | | |
| 22 | * | | | 78 | LBL 13 | | |
| 23 | PI | | | 79 | RCL 02 | | |
| 24 | * | | | *80 | "L=" | | |
| 25 | STO 00 | | $2\pi d \rightarrow R_{00}$ | *81 | PRA | | |
| 26 | "SIL HT?" | | | *82 | PRX | | |
| 27 | PROMPT | | | 83 | 1/X | | |
| *28 | "SIL HT=" | | | 84 | RCL 00 | | |
| *29 | PRA | | | 85 | * | | |
| *30 | PRX | | | 86 | 2 | | |
| 31 | STO 08 | | $h \rightarrow R_{08}$ | 87 | * | | $4\pi d/L \rightarrow R_{06}$ |
| 32 | "PERIOD?" | | | 88 | STO 06 | | |
| 33 | PROMPT | | | 89 | XEQ 03 | | |
| *34 | "PERIOD=" | | | 90 | RCL 06 | | |
| *35 | PRA | | | 91 | + | | |
| *36 | PRX | | | 92 | STO 07 | | $R_{06} + \sinh(R_{06}) \rightarrow R_{07}$ |
| 37 | X12 | | | 93 | 4 | | |
| 38 | RCL 06 | | | 94 | ENTER+ | | |
| 39 | * | | | 95 | PI | | |
| 40 | 2 | | | 96 | * | | |
| 41 | / | | | 97 | RCL 08 | | |
| 42 | PI | | | 98 | * | | |
| 43 | / | | | 99 | RCL 02 | | |
| 44 | STO 01 | | $L_0 \rightarrow R_{01}$ | 100 | / | | |
| 45 | LBL "ITERAT" | | | 101 | STO 09 | | |
| 46 | STO 03 | | $L_{old} \rightarrow R_{03}$ | 102 | XEQ 03 | | $\frac{4\pi h}{L} \rightarrow R_{09}$ |
| 47 | 1/X | | | 103 | RCL 09 | | |
| 48 | PCL 00 | | | 104 | + | | |
| 49 | * | | | 105 | RCL 07 | | |
| 50 | STO 04 | | | 106 | / | | |
| 51 | END | | | 107 | CHS | | |
| 52 | PCL 04 | | $\frac{2\pi d}{L_{old}} \rightarrow R_{04}$ | 108 | 1 | | |
| 53 | CHS | | | 109 | + | | |
| 54 | END | | | 110 | SORT | | $H_t/H_i = K_t$ in display |
| 55 | - | | | *111 | "KT=" | | |
| 56 | PCL 04 | | | *112 | PRA | | |
| | | | | *113 | PRX | | |

*THESE LINES MUST BE DELETED IF A PRINTER IS NOT AVAILABLE.

105R-41CV-3

Program Listing

[illegible]

105R-41CV-4

* THESE LINES MUST BE DELETED IF A PRINTER IS NOT AVAILABLE.

APPENDIX
BLANK PROGRAM FORMS

Program Description

| | | |
|--|--------------|-----------------|
| Program Title | | |
| Name | Date | |
| Address | | |
| City | State | Zip Code |
| Program Description, Equations, Variables, etc. | | |
| Operating Limits and Warnings | | |

User Instructions

Program Title

[illegible]

Program Listing

| STEP | KEY ENTRY | KEY CODE | COMMENTS | STEP | KEY ENTRY | KEY CODE | COMMENTS |
|------|-----------|----------|----------|------|-----------|----------|----------|
| 001 | | | | | | | |
| | | | | | | | |
| | | | | 060 | | | |
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|--|--|
| <p>Walton, Todd L. Hand-held calculator algorithms for coastal engineering (second series) / by Todd L. Walton, Jr.--Fort Belvoir, Va. : U.S. Army, Corps of Engineers, Coastal Engineering Research Center ; Springfield, Va. : available from NTIS, 1982. [41] p. : 27 cm.--(Coastal engineering technical aid ; no. 82-4) Cover title. "November 1982." This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation. Six programs are included for use with HP41CV hand-held calculators which employ the Reverse Polish Notation (RPN). These programs can be used to compute linear wave parameters, orbital velocities, breaking wave height and direction, shallow-water wave forecasts, depth-limited breaking wave height, and wave transmission past a vertical barrier. 1. Calculator algorithms. 2. Coastal engineering. 3. Wave generation. 4. Wave transformation. I. Title. II. Series. TC203 .U581ta no. 82-4 627</p> | <p>Walton, Todd L. Hand-held calculator algorithms for coastal engineering (second series) / by Todd L. Walton, Jr.--Fort Belvoir, Va. : U.S. Army, Corps of Engineers, Coastal Engineering Research Center ; Springfield, Va. : available from NTIS, 1982. [41] p. : 27 cm.--(Coastal engineering technical aid ; no. 82-4) Cover title. "November 1982." This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation. Six programs are included for use with HP41CV hand-held calculators which employ the Reverse Polish Notation (RPN). These programs can be used to compute linear wave parameters, orbital velocities, breaking wave height and direction, shallow-water wave forecasts, depth-limited breaking wave height, and wave transmission past a vertical barrier. 1. Calculator algorithms. 2. Coastal engineering. 3. Wave generation. 4. Wave transformation. I. Title. II. Series. TC203 .U581ta no. 82-4 627</p> |
| <p>Walton, Todd L. Hand-held calculator algorithms for coastal engineering (second series) / by Todd L. Walton, Jr.--Fort Belvoir, Va. : U.S. Army, Corps of Engineers, Coastal Engineering Research Center ; Springfield, Va. : available from NTIS, 1982. [41] p. : 27 cm.--(Coastal engineering technical aid ; no. 82-4) Cover title. "November 1982." This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation. Six programs are included for use with HP41CV hand-held calculators which employ the Reverse Polish Notation (RPN). These programs can be used to compute linear wave parameters, orbital velocities, breaking wave height and direction, shallow-water wave forecasts, depth-limited breaking wave height, and wave transmission past a vertical barrier. 1. Calculator algorithms. 2. Coastal engineering. 3. Wave generation. 4. Wave transformation. I. Title. II. Series. TC203 .U581ta no. 82-4 627</p> | <p>Walton, Todd L. Hand-held calculator algorithms for coastal engineering (second series) / by Todd L. Walton, Jr.--Fort Belvoir, Va. : U.S. Army, Corps of Engineers, Coastal Engineering Research Center ; Springfield, Va. : available from NTIS, 1982. [41] p. : 27 cm.--(Coastal engineering technical aid ; no. 82-4) Cover title. "November 1982." This report provides algorithms for a number of calculator programs useful in performing coastal engineering calculations, primarily in the area of wave transformations and wave generation. Six programs are included for use with HP41CV hand-held calculators which employ the Reverse Polish Notation (RPN). These programs can be used to compute linear wave parameters, orbital velocities, breaking wave height and direction, shallow-water wave forecasts, depth-limited breaking wave height, and wave transmission past a vertical barrier. 1. Calculator algorithms. 2. Coastal engineering. 3. Wave generation. 4. Wave transformation. I. Title. II. Series. TC203 .U581ta no. 82-4 627</p> |

